

$$11.1 \text{ Moment of Inertia Tensor } I_{ij} = \int \rho(\vec{r}) [d_{ij} \cdot \sum_k x_k^2 - x_i x_j] dV$$

For a homogeneous sphere of radius R

$$\begin{aligned} I_{33} &= \rho \int (r^2 - z^2) dV \\ &= \rho \int_0^R \int_0^\pi \int_0^{2\pi} (r^2 - r^2 \cos^2 \theta) r^2 \sin \theta d\phi d\theta dr \\ &= 2\pi \rho \int_0^R r^4 dr \int_{-1}^1 (1 - u^2) du \quad \text{where } u = \cos \theta \\ &= 2\pi \rho \frac{R^5}{5} \left(u - \frac{u^3}{3} \right) \Big|_{-1}^1 \\ &= \frac{8\pi \rho R^5}{15} \end{aligned}$$

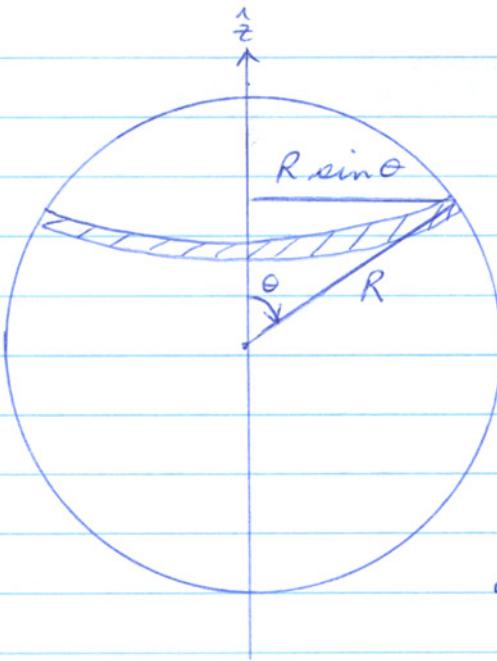
$$\therefore I_{33} = \frac{2}{5} MR^2 \text{ using } M = \rho \frac{4}{3}\pi R^3$$

By symmetry $I_{11} = I_{22} = I_{33}$. The off diagonal elements are zero. For example:

$$\begin{aligned} I_{12} &= \rho \int -xy dV \\ &= \rho \int_0^R \int_0^\pi \int_0^{2\pi} r^2 \sin^2 \theta \sin \phi \cos \phi r^2 \sin \theta d\phi d\theta dr \\ &= 0 \end{aligned}$$

Hence \underline{I} is a diagonal matrix and the principal moments are $I_1 = I_2 = I_3 = \frac{2}{5} MR^2$.

11.6



Consider a ring of spherical shell.

Area of ring is $R d\theta = \pi R \sin \theta$

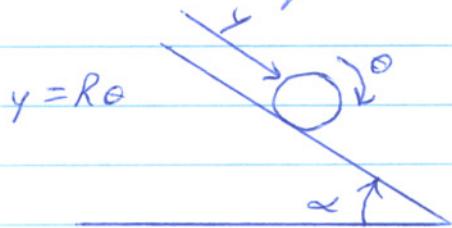
mass of ring is $\sigma = \pi R^2 \sin \theta d\theta$
density

∴ Moment of Inertia for rotation
about \hat{z} axis is:

$$\begin{aligned} I &= \int_0^\pi (R \sin \theta)^2 \sigma 2\pi R^2 \sin \theta d\theta \\ &= \int_0^\pi \sigma R^4 \int_0^\pi \sin^3 \theta d\theta \\ &= \frac{8\pi}{3} \sigma R^4 \end{aligned}$$

$$\therefore I = \frac{2}{3} M R^2 \text{ where } M = \sigma 4\pi R^2$$

The two spheres will now be rolled down an inclined plane.



$$\text{Kinetic Energy } T = \frac{M}{2} \dot{\gamma}^2 + \frac{I}{2} \dot{\theta}^2$$

$$= \left(\frac{M}{2} + \frac{I}{2R^2} \right) \dot{\gamma}^2$$

$$\text{Potential Energy } U = -M g y \sin \alpha$$

$$\text{Lagrangian } L = \left(M + \frac{I}{R^2} \right) \dot{\gamma}^2 + M g y \sin \alpha$$

$$\text{Egn. of Motion } \frac{dL}{dy} - \frac{d}{dt} \left(\frac{\partial L}{\partial \dot{y}} \right) = 0$$

$$Mg \sin\alpha - \left(M + \frac{I}{R^2} \right) \ddot{y} = 0$$

$$\ddot{y} = g \frac{MR^2 \sin\alpha}{MR^2 + I}$$

But I (solid sphere) $<$ I (spherical shell)

\therefore solid sphere has greater acceleration down inclined plane than spherical shell of same mass & radius.

11.13 Moment of Inertia tensor is:

$$I_{ij} = \sum_{\alpha} m_{\alpha} \left[\delta_{ij} \sum_k x_{\alpha k}^2 - x_{\alpha i} x_{\alpha j} \right]$$

$$\therefore I_{11} = \sum_{\alpha} m_{\alpha} \left[x_{\alpha 1}^2 + x_{\alpha 3}^2 \right]$$

$$= 3mb^2 + 4m(zb^2) + 2mb^2 \\ = 13mb^2$$

$$\text{Similarly } I_{22} = 16mb^2 \text{ & } I_{33} = 15mb^2.$$

$$I_{12} = I_{21} = - \sum_{\alpha} m_{\alpha} x_{\alpha 1} x_{\alpha 2}$$

$$= -3m0 - 4mb^2 - 2m(-b^2) \\ = -2mb^2$$

$$\text{Similarly } I_{23} = I_{32} = 4mb^2 \text{ & } I_{13} = I_{31} = mb^2.$$

$$\therefore \underline{\underline{I}} = mb^2 \begin{pmatrix} 13 & -2 & 1 \\ -2 & 16 & 4 \\ 1 & 4 & 15 \end{pmatrix}$$

The principal moments of inertia are found solving:

$$\begin{vmatrix} 13-\lambda & -2 & 1 \\ -2 & 16-\lambda & 4 \\ 1 & 4 & 15-\lambda \end{vmatrix} = 0$$

$$\text{OR } \lambda^3 - 44\lambda^2 + 622\lambda - 2820 = 0$$

This has solutions (found numerically) $\lambda_1 = 10$, $\lambda_2 = 14.35$
 $+ \lambda_3 = 19.65$

∴ principal moments of inertia are $I_1 = 10 \text{ mb}^2$, $I_2 = 14.35 \text{ mb}^2$
 $+ I_3 = 19.65 \text{ mb}^2$.

Principal axes are found solving $(I - \omega I_i) \vec{\omega} = 0$.

$$I_i = I_1 \Rightarrow \begin{pmatrix} 13-10 & -2 & 1 \\ -2 & 16-10 & 4 \\ 1 & 4 & 15-10 \end{pmatrix} \begin{pmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

$$\text{OR } 3\omega_1 - 2\omega_2 + \omega_3 = 0 \quad (1)$$

$$-2\omega_1 + 6\omega_2 + 4\omega_3 = 0 \quad (2)$$

$$\omega_1 + 4\omega_2 + 5\omega_3 = 0. \quad (3)$$

(1) $\Rightarrow \omega_3 = -3\omega_1 + 2\omega_2$ Substituting this into (2) gives:

$$-2\omega_1 + 6\omega_2 + 4(-3\omega_1 + 2\omega_2) = 0,$$

$$\therefore \omega_1 = \omega_2$$

$$\text{Then (3)} \Rightarrow \omega_3 = -\omega_2.$$

∴ principal axis associated with I_1 is $\frac{1}{\sqrt{3}}(\hat{x} + \hat{y} - \hat{z})$

Similarly principal axes associated with I_2 is $.81\hat{x} + .29\hat{y} - .52\hat{z}$
 " " " I_3 " $-.14\hat{x} + .77\hat{y} + .63\hat{z}$

Note that the 3 principal axes are perpendicular.

11.20



Upright rod has total energy

$$\begin{aligned} E &= \text{Potential Energy} \\ &= mg \frac{b}{2} \end{aligned} \quad (1)$$

When rod hits floor, total energy

$$\begin{aligned} E &= \text{Kinetic Energy} \\ &= \frac{I}{2} \omega^2 \end{aligned} \quad (2)$$

Moment of Inertia of uniform rod about an end is

$$I = \int_0^b x^2 \sigma dx = \sigma \frac{b^3}{3} = \frac{mb^2}{3} \quad (3) \quad \text{where } m = \sigma b$$

Combining (1), (2) & (3) gives:

$$mg \frac{b}{2} = \frac{mb^2}{3} \omega^2$$

$\therefore \omega = \sqrt{\frac{3g}{b}}$ is angular velocity of rod when hitting the floor.

11.29 For a vertical top ($\theta=0, \dot{\theta}=0$) we have the following

$$(11.153 + 11.154) \Rightarrow p_\phi = p_\psi = I_3 (\dot{\phi} + \dot{\psi})$$

$$(11.159) \Rightarrow p_\phi = p_\psi = I_3 \omega_3$$

$$(11.160) \Rightarrow E' = Mgh$$

This problem seeks to examine the stability of the top near $\theta=0$. Substituting Mgh for E' in 11.160 gives:

$$Mgh = \frac{I_1}{2} \dot{\theta}^2 + \frac{I_3^2 \omega_3^2 (1 - \cos\theta)^2}{2 I_1 \sin^2\theta} + Mgh \cos\theta$$

We now set $z \equiv \cos\theta \therefore \dot{z} = -\sin\theta \dot{\theta}$

$$\dot{\theta}^2 = \frac{\dot{z}^2}{\sin^2\theta} = \frac{\dot{z}^2}{1 - \cos^2\theta} = \frac{\dot{z}^2}{1 - z^2}$$

$$\therefore Mgh = \frac{I_1}{2} \frac{\dot{z}^2}{1 - z^2} + \frac{I_3^2 \omega_3^2 (1 - z)^2}{2 I_1 (1 - z^2)} + Mghz$$

$$Mgh(1 - z) = \frac{I_1}{2} \frac{\dot{z}^2}{1 - z^2} + \frac{I_3^2 \omega_3^2 (1 - z)^2}{2 I_1 (1 - z^2)}$$

Multiplying by $2 I_1 (1 - z^2)$ gives:

$$2 I_1 Mgh(1 - z)(1 - z^2) = I_1^2 \dot{z}^2 + I_3^2 \omega_3^2 (1 - z)^2$$

$$I_1^2 \dot{z}^2 = (1 - z)^2 [2 I_1 Mgh(1 + z) - I_3^2 \omega_3^2]$$

$$\dot{z}^2 = \frac{(1 - z)^2}{I_1^2} [2 I_1 Mgh(1 + z) - I_3^2 \omega_3^2] \quad (1)$$

Obviously $\dot{z}^2 \geq 0$.

Case 1: w_3 is large such that $2I_1Mgh(1+z) - I_3^2 w_3^2 < 0$

$$\Rightarrow z=1 \Rightarrow \theta=0$$

\therefore motion is stable if $4I_1Mgh - I_3^2 w_3^2 < 0$

Case 2: w_3 is small such that $2I_1Mgh(1+z) - I_3^2 w_3^2 > 0$

$\Rightarrow \ddot{z}^2 > 0 \Rightarrow \theta$ increases from 0. This continues until $z=z_0$ such that $2I_1Mgh(1+z_0) - I_3^2 w_3^2 = 0$.

\therefore there is nutation between $z=1 + z=z_0$.

\therefore there is a critical angular frequency w_c such that
 $w_3 > w_c \Rightarrow$ stable motion
 $w_3 < w_c \Rightarrow$ nutation

where $2I_1Mgh - I_3^2 w_c^2 = 0$

$$w_c = \frac{2}{I_3} \sqrt{MghI_1}$$

Hence, if top starts with $w_3 > w_c$ & $\theta=0^\circ$, motion is stable. As friction slows the top w_3 reduces and at $w_3 = w_c$, nutation starts.